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COMPUTER PROGRAMS FOR CALCULATION OF MATRIX STABILITY AND FREQUENCY RESPONSE FROM A STATE-SPACE SYSTEM DESCRIPTION

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# ABSTRACT

FORTRAN computer subroutines stemming from requirements to process state variable system equations for systems of high order are presented. They find the characteristic equation of a matrix using the method of Danilevsky, the number of roots with positive real parts using the Routh-Horwitz alternate formulation, convert a state variable system description to a Laplace transfer function using the method of Bollinger, and evaluate that transfer function and obtain its frequency response. A sample problem is presented to demonstrate use of the subroutines.

# COMPUTER PROGRAMS FOR CALCULATION OF MATRIX STABILITY AND

FREQUENCY RESPONSE FROM A STATE-SPACE SYSTEM DESCRIPTION

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### SUMMARY

FORTRAN computer subroutines stemming from requirements to process state variable system equations for systems of high order are presented. They find the characteristic equation of a matrix using the method of Danilevsky, the number of roots with positive real parts using the Routh-Horwitz alternate formulation, convert a state variable system description to a Laplace transfer function using the method of Bollinger, and evaluate that transfer function and obtain its frequency response. A sample problem is presented to demonstrate use of the subroutines.

# INTRODUCTION

High-speed digital computers have made matrix state variable methods for system analysis practical. But for large systems, the required execution time and the cumulative effect of round off errors make it increasingly important to employ efficient algorithms. FORTRAN subroutines resulting from requirements to handle large systems are reported herein. In particular, they find the characteristic equation of a system matrix, test that equation for the number of roots with positive real parts, convert a state variable system description to a Laplace transfer function and evaluate the transfer function at a given frequency to obtain its frequency response.

The FORTRAN program for obtaining the characteristic equation of a system matrix uses the method of Danilevsky, reference 1. The program includes a Gauss pivotal element condensation scheme to somewhat increase its accuracy. A competing method is that of Leverrier, references 1 and 2. However, to compute the characteristic polynomial the Danilevsky method is known to be more accurate, faster, and require less storage. The FORTRAN program for determining the stability of the characteristic polynomial uses the Routh-Horwitz alternate formulation method, reference 3. The FORTRAN program for obtaining the system transfer function uses the method of Bollinger, reference 4. This method appears more reliable than the method of Davison, reference 5, which in certain cases is known to converge improperly (ref. 4). However Davison's transformation, which permits the output to be an arbitrary linear combination of the states, is used in

conjunction with Bollinger's method. The inverse of this transformation is also required, but is easily calculated in closed form. Once the transfer function is obtained its frequency response is easily calculated.

The FORTRAN listings and subroutine descriptions are presented in the following section. Equation symbols are defined in Appendix A. FORTRAN symbols are defined separately for each program. A sample problem demonstrating the use of the subroutines is described in Appendix B.

#### COMPUTER PROGRAMS

# Characteristic Equation

In subroutine DANSKY the characteristic equation of a matrix is found by the method of Danilevsky, reference 1. The characteristic equation of an nxn matrix A is an expansion of the determinant equation

$$|A - \lambda I| = (-1)^n (\lambda^n + Z1_1 \lambda^{n-1} + \cdots + Z1_n) = 0$$

where I is the identity matrix and the polynomial coefficients sought are in the Z1 vector. The Z1 vector coefficients are obtained in DANSKY through successive application of similarity transformations which finally produce the Zl vector in the top row of A. As noted in reference 1 the method allows use of a Gauss pivotal element scheme to somewhat increase its accuracy. In DANSKY this option is implemented. The Gauss method performs similarity transformations which interchange columns and rows of A to place the element with the largest absolute value in pivot position. The execution time for an 18x18 A matrix is about 0.35 sec (IBM-360-67 TSS computer). DANSKY uses (as most of the programs) double precision. The time penalty for using double precision is only about 0.02 sec for the 18x18 matrix. One problem which occurs with certain A matrices when using DANSKY is that of exponent under or overflow. In such cases the matrix A may be (time) scaled by multiplying each element of A by a positive constant, r. The characteristic polynomial of the scaled matrix becomes

$$\lambda^n + (z1_1r)\lambda^{n-1} + \cdots + (z1_nr^n)$$

Figure 1 is a description of the DANSKY calling statement transfer variables. Figure 2 is a FORTRAN listing of DANSKY.

For comparison with the Danilevsky method some results obtained with the Leverrier method are cited. For the same 18x18 matrix discussed earlier, the Leverrier program required 4.2 sec (compared to 0.35 sec for the Danilevsky method). Also, two additional 18x18 double precision scratch storage matrices are required for the Leverrier method, and double precision is required to obtain the same accuracy achieved by DANSKY in single precision.

In DANSKY a call is made to subroutine POLMPY to multiply two polynomials. In certain cases the method of Danilevsky obtains the characteristic equation coefficients in partially factored form and the factors must be multiplied together to obtain the characteristic equation. In DANSKY a call is made to POLMPY in all cases with one of the polynomials possibly unity. Figure 3 is a description of the POLMPY transfer variables. Figure 4 is a FORTRAN listing of POLMPY.

# Stability

The subroutine RHWTZ performs a stability test upon the characteristic equation. It counts the number of roots with positive real parts without actually finding them. A simple recursive algorithm which is well suited to machine computation is used. Its description is given in reference 3. The program is specialized in that it assumes the leading polynomial coefficient is unity as in the form returned by DANSKY. The execution time for an eighteenth order polynomial is about 0.007 sec. Figure 5 presents a description of the RHWTZ transfer variables and figure 6 presents a FORTRAN listing of RHWTZ.

For certain equations the test may fail if during the algorithm execution a zero appears as a divisor term. In this case the number of unstable roots is set to -1 and the message "Test Failed M set to -1" is output.

### Transfer Function

BOLLIN is a subroutine for converting a state variable matrix differential equation into an equivalent Laplace transfer function. The system equations considered are

$$\dot{x} = Ax + Bu, y = C^{t}x$$

where x, B, and C are n vectors, A is an  $n \times n$  matrix, and u and y are input and output scalars. The following steps are taken to obtain the system transfer function:

1. A call to subroutine DAVISO transforms the A and B system matrices using the C vector so as to make the output y a state variable in the transformed system, reference 5. The transformed system is

$$A^* = TAT^{-1}$$
,  $B^* = TB$ , and  $x^* = Tx$ 

such that

$$\overset{\circ}{x} = \overset{\star}{A}\overset{\star}{x} + \overset{\star}{B}^{u}$$

where T is the identity matrix except that the MC-th row is overwritten by the C<sup>t</sup> vector. The integer MC is the position of the element of C with the maximum absolute value. The  $T^{-1}$  matrix is similar to inverses encountered in the proof of the Danilevsky method, reference 1, and can be written down explicitly. The output  $Y^*$  of the modified system is the MC-th modified state variable,  $X_{MC}$ .

- 2. The denominator polynomial Z1 (characteristic equation) of the system transfer function is obtained by a call to DANSKY using the  $\mathbf{A}^*$  matrix.
- 3. The numerator polynomial is obtained in two more calls to DANSKY using Bollinger's method, reference 4. First, with the MC-th column of A replaced by -B to obtain Z2; then, with a matrix of order (n-1) obtained by deleting the MC-th row and column from A to obtain Z3.
  - 4. The numerator polynomial is computed as Z4 = Z2 sZ3.
  - 5. The system transfer function y(s)/u(s) is Z4(s)/Z1(s).

Execution times found for various order systems were about 1.0 sec for an eighteenth order, 2.7 sec for a twenty-sixth order, and 9.7 sec for a forty-first order system. Figure 7 is a description of the BOLLIN transfer variables. Figure 8 is a FORTRAN listing of BOLLIN. Figure 9 is a description of the DAVISO transfer variables and figure 10 is a FORTRAN listing of DAVISO. If the A matrix is time scaled by multiplication by scalar r, the B vector and frequencies used to evaluate the transfer function should also be scaled by r. To handle the more general case of multiple input, multiple output systems where B and C are matrices, the program calling BOLLIN would start the B and C matrices at the appropriate columns in the transfer variable list to obtain the desired input/output relation, reference 5.

# Frequency Response

The subroutine FRPOLY may be used to evaluate the Laplace transform Z4(s)/Z1(s) ratio of polynomials for a given frequency  $s=j\omega$ . The evaluation is performed in double precision with the real and imaginary parts of the powers of  $j\omega$  handled separately. Figure 11 is a description of the FRPOLY transfer variables and figure 12 is a FORTRAN listing of FRPOLY. To evaluate a system frequency response over a range of frequencies, multiple calls to FRPOLY would be made.

#### CONCLUDING REMARKS

Six subroutines: DANSKY, POLMPY, RHWTZ, BOLLIN, DAVISO, and FRPOLY were presented and discussed. The chart shown in figure 13 summarizes the flow from a state variable representation of a system through the various subroutines. The major input and output relations and alternate paths for various uses are noted.

#### REFERENCES

- 1. Faddeeva, V. N.: Computational Methods of Linear Algebra. Dover Publications, 1959, pp. 166-176.
- 2. Zadeh, Lotfi A., and Desoer, Charles A.: Linear System Theory; The State Space Approach. McGraw-Hill Book Co., Inc., 1963, pp. 303-305.
- 3. Korn, Gravins A., and Korn, Theresa M.: Mathematical Handbook for Scientists and Engineers. 2nd ed., McGraw-Hill Book Co., Inc., 1961.
- 4. Bollinger, K. E., and Mathur, J. C.: To Compute the Zeros of Large Systems. IEEE Trans., vol. AC-16, no. 1, Feb. 1971, pp. 95-96.
- 5. Davison, E. J.: A Computational Method for Finding the Zeros of a Multivariable Linear Time Invariant System. Automatica, vol. 6, no. 3, May 1970, pp. 481-484.

## APPENDIX A

# SYMBOLS

- A system matrix, nxn
- B input vector, n
- C output vector, n
- I identity matrix, nxn
- j imaginary,  $\sqrt{-1}$
- MC position of element in C with maximum absolute value
- n system order
- r scaling factor
- s Laplace variable, sec-1
- t time, sec
- T transformation matrix, nxn
- u input
- x state variable vector, n
- y output
- Zl characteristic equation polynomial
- Z2 intermediate polynomial
- Z3 intermediate polynomial
- Z4 system numerator transfer function polynomial
- λ root of characteristic equation
- ω frequency, hertz

# Superscript:

- \* denotes transformed variable
- t transpose

#### APPENDIX B

#### SAMPLE PROBLEM

A third order sample problem demonstrating the combined use of the subroutines is described next. The problem studied is the transfer function

$$\frac{y(s)}{u(s)} = \frac{s+6}{(s^2+3s+9)(s+4)} = \frac{s+6}{s^3+7s^2+21s+36}$$

In phase variable form the state matrices are

$$A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -36 & -21 & -7 \end{bmatrix}, B = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}, C = \begin{bmatrix} 6 \\ 1 \\ 0 \end{bmatrix}$$

Figure 14 is a FORTRAN listing of the sample problem MAIN program. First the A, B, and C matrices are output. Next after a call to BOLLIN, the denominator and numerator polynomial coefficients are output. Then, after a call to FRPOLY, the transfer function evaluated at one hertz is output, and finally, after a call to RHWTZ, the number of unstable roots is output.

Figure 15 is a listing of the program output. The denominator polynomial is  $s^3+7s^2+21s+36$  with the unity coefficient of  $s^3$  understood. The numerator polynomial is -2.220E-16 s $^2+s+6$ . The coefficient of the  $s^2$  term should actually be zero but due to limited numerical precision is slightly in error. The transfer function is evaluated at one hertz ( $s=j2\pi$ ) and has a real part of -.03048 and an imaginary part of -.01142 or an amplitude of .03255 at -159.5 degrees. There are no roots of the denominator polynomial with positive real parts.

If only a test of system stability were desired then it would not be necessary to use BOLLIN. Instead DANSKY could be called to obtain the characteristic equation followed by a call to RHWTZ. BOLLIN is organized such that it computes the denominator transfer function Z1 each time it is called. To save computations the user may wish to modify this if the transformed matrix A is known to remain constant for a particular set of B and/or C changes.

## DANSKY

Danilevsky

PURPOSE: To obtain the characteristic equation of a

square real matrix

USAGE: CALL DANSKY (A, X, Y, Z, N, NMAX)

Where A - square real matrix, order NxN

X - scratch vector, order N

Y - scratch vector, order N

Z - characteristic polynomial vector, order N

N - order of A

NMAX - dimension of A in calling program > N

DOUBLE DIMENSION: A must be double dimen-

sioned (NMAX, NMAX) in

calling program

DOUBLE PRECISION: A, X, Y, and Z must be

double precision in calling

program

NOTES: (1) A is destroyed in obtaining Z

(2) The Z characteristic equation is returned in the form

 $\lambda^{n} + z_{1}\lambda^{n-1} + \cdots + z_{n-1}\lambda + z_{n}$ 

Subroutines called: (1) POLMPY

FIGURE 1.-DESCRIPTION OF SUBROUTINE DANSKY TRANSFER VARIABLES

```
COMPUTE THE COSEFICIENTS OF THE CHARACTERISTIC ECUATION
        SUBROUTINE DANSKY(A, X, Y, Z, N, NMAX)
DIMENSION A(NMAX, 1), X(1), Z(1), Y(1)
        DOUBLE PRECISION SUM, A, SAVE, PIVOT, CK, X, Y, Z
        NM1=NN-1
10
       IF(NM1.EQ.0) GO TO 125
DO 120 I=1, NM1
       NMI = NN = I
        I PVT=NMI
        NMIMI=NMI-1
        NM1 P1=NM1+1
   FIND MAXIMUM ELEMENT IN PIVOT ROW
        XMAX=A(NMIP1,NMI)
        (F(NPM1.GT.0) GO TO 15
        IF(XMAX, EQ. 0.) GO TO 140
        00 TO 50
        DO 20 K1=1,NMIM1
15
        K=NMI-KI
        IF(ABS(SMGL(A(NMIPI,K))).LE.ABS(XMAX)) OF TO RE
        XMAX=A(NM1P1,K)
        1PVT=K
        CONTINUE
20
        IF(XMAX.EQ.0.) GO TO 140
   IF(1PVT.EQ.MMI) GO TO 50
SIMULARITY TRANSFORM SO PIVOT ELEMENT IS THE MAXIMUM
        DO 30 J=1,NMIP1
        SAVE=A(J, IPVT)
A(J, IPVT)=A(J, NMI)
        AVA=(IMM,U)∧
30
        DO 40 JJI, NN
SAVE=A(IPVT,J)
        (L,1MM)A=(b,TV91)A
   A(NMI,J) = SAVE
A UPDATE EQUALS A + M(SUB N-1)
40
C
        PIVOT=1./A(NM1P1,NM1)
50
        DO 80 K#1,NN
        IF (K.EO.NMI) NO TO 80
        CK--A(NMIP1,K)+PIVOT
        DO 70 ||=1,NM|
A(||,K)=A(||,K)+A(||,NM|)*6K
70
8-0
        CONTINUE
   DO 85 [[=1,NM]
A(11,NM1)=A(11,NM1)=PIVOT
MULT M(SUB N=1) INVERSE TIMES A UPPATED
DO 110 11=1,NM
85
        SUM=0.
DO 90 K=1,NMI
SUM=SUM+A(NMIPI,K)*A(K,II)
IF(II.LT.NMI) AA TO 100
90
        IF(II, EQ.NN) NO TO 100
        SUM=SUM+A(NMIP1, II+1)
        IF(||.LT.NM|) AA TO 100
|F(||.EQ.NN) AO TO 100
SUM=SUM+A(NN||P1,||+1)
        A(NMI, LI)=8UM
CONTINUE
100
110
120
        CONTINUE
        NMI P1=1
125
    ELEMENTS OF C SET ECUAL TO LAST ELEMENTS IN ROW MMIP1 OF #A
140
        DO 150 J≡NMIP1,NN
        NX=J=NMIP1+1
    ) X(NX)==A(NMIP1,U)
MULTIPLY OUT FACTORS OF CHARACTERISTIC FOUATION
150
<u>190</u>
        NY=N=NN
        PO 200 J=1,NY
Y(J)=Z(J)
200
    GALL POLIPPY(X,Y,Z,NX,NY,NYPNX)
REDUCE SYSTEM ORNER
        NN=NN=NX
         1F(NN.6T.0) 60 TO 10
        RETURN
         END
```

# POLMPY

# Polynomial Multiplication

PURPOSE:

To multiply two polynomials X\*Y

CALL POLMPY (X, Y, Z, NX, NY, NZ)

Where

X - first polynomial, vector

Y - second polynomial, vector

Z - returned product polynomial, vector

NX - order of X

NY - order of Y

NZ = NX + NY (order of Z) returned

NOTE: (1) leading coefficient of highest power is assumed to be one, i.e., for X:

$$\lambda^{\text{NX}} + x_1 \lambda^{\text{NX}-1} + \cdots + x_{\text{NX}}$$

DOUBLE PRECISION: X, Y, and Z must be double precision in the calling program

FIGURE 3.-DESCRIPTION OF SUBROUTINE POLMPY TRANSFER VARIABLES

```
C MULTIPLY X*Y=Z (LEADING POLYNOMIAL COEFFICIENTS ASSUMED UNITY)
       SUBROUTINE POLMPY(X,Y,Z,NX,NY,NZ)
      DIMENSION X(1), Y(1), Z(1)
DOUBLE PRECISION X, Y, Z, YJ
       NZ=NX+PY
   IF NX=0 MEANS POLY X=1; THEREFORE Z=Y
       IF(NX.GT.O) GO TO 6
       DO 4 J=1,NY
       Z(J)=Y(J)
4
       GO TO 40
   IF NY=0 MEANS POLY Y=1; THEREFORE Z=X IF(NY.ST.0) GO TO 15 DO 8 J=1,NX
6
       Z(J)=X(J)
8
       GO TO 40
   START MULTIPLICATION BY MAKING Z=Y*S**NX
       DO 20 J=1,NZ
15
       (L)Y=LY
       IF(J.GT.NY) YJ=0.
20
       Z(J)=YJ
   MULTIPLICATION LOOP
С
       DO 30 K=1,NX
       Z(K)=Z(K)+X(K)
       DO 25 J=1,NY
       KPJ=K+J
       Z(KPJ)=Z(KPJ)+Y(J)*X(K)
25
       CONTINUE
30
       RETURN
40
        END
```

# RHWTZ

### ROUTH - HURWITZ ALTERNATE FORMULATION

PURPOSE:

To compute the number of roots with positive real

parts of a polynomial equation

USAGE:

CALL RHWTZ (C,N,M)

Where

C - coefficients of polynomial equation, vector

N - equation order

M - number of roots with positive real parts (M set to -1 if test fails due to attempted)

division by zero)

RESTRICTION:

The C vector starts with the second coefficient, as the first is assumed unity; that is:

 $\lambda^{n} + c_{1}\lambda^{n-1} + \cdots + c_{n-1}\lambda + c_{n} = 0$ 

NOTE: C is destroyed upon return

DOUBLE PRECISION: C must be double precision

in the calling program

PROGRAM OUTPUT: "TEST FAILED M SET TO -1" out-

put if division by zero is

attempted

FIGURE 5.-DESCRIPTION OF SUBROUTINE RHWTZ TRANSFER VARIABLES

```
ROUTH HORVITZ ALTERNATE FORMULATION STABILITY TEST SUBROUTINE RHUTZ(C,N,M) DOUBLE PRECISION C,CNM1,COEF,CNM2
       DIMENSION C(1)
       NM1=N-1
       M≠O
   PROVIDE FOR CASE N=0,1,0R 2
C -
       IF(N.LE.0) GO TO 30
       IF(N-2) 4,8,10
IF(C(1).LT.0.) M=1
       GO TO 30
8
       CNM1=1.
       GO TO 25
       ** (C(1).EQ.O.) GO TO 35
10
       COEF=1./C(1)
   START ALGORITHM LOOP
       DO 20 K=2,NM1
       IF(COEF.LT.0) M=M+1
       DO 15 J=K,NM1,2
       C(J)=C(J)-COEF+C(J+1)
1F(C(K).EQ.O.) GO TO 35
15
       COEF=C(K-1)/C(K)
       CONTINUE
20
    FINISH REMAINING 2 ND ORDER POLYNOMIAL
       CNM2=C(N-2)
        IF(CNM2+C(NM1).LT.0.) M=M+1
25
23
        1F(C(NM1) +C(N).LT.0.) M=M+1
30
       RETURN
       WRITE(6,45)
35
        FORMAT(1X, 23HTEST FAILED M SET TO -1)
45
        M = -1
        GO TO 30
        END
```

### BOLLIN

Bollinger

PURPOSE:

To obtain a system transfer function from system

matrix equations

**USAGE:** 

CALL BOLLIN (A,AS,B,X,Y,Z1,Z2,Z3,N,NMAX)

Where

A - system matrix (NxN)

AS - scratch matrix (NxN)

B - system input vector (N)

C - system output vector (N)

X - scratch vector (N)

Y - scratch vector (N)

Z1 - transfer function denominator, vector (N)

Z2 - transfer function numerator, vector (N)

Z3 - scratch, vector (N)

N - system order

NMAX - dimension of A and AS in calling program > N

DOUBLE DIMENSION: A and AS must be double

dimensioned (NMAX, NMAX)

in calling program

DOUBLE PRECISION: AS must be double precision

in calling program

NOTES: (1) A is destroyed in obtaining Z1 and Z2

(2) The Z1 and Z2 are returned as in

$$Z1 = \lambda^{n} + Z1_{1}\lambda^{n-1} + \cdots + Z1_{n}$$

$$z2 = z2_1\lambda^{n-1} + \cdots + z2_n$$

SUBROUTINES CALLED: (1) DAVISO

(2) DANSKY

FIGURE 7.-DESCRIPTION OF SUBROUTINE BOLLIN TRANSFER VARIABLES

```
CONVERT X(DOT)=AX+BU,Y=C(TRANSPOSE)X TO TRANSFER
C
   FUNCTION Y/U=Z2/Z1 RATIO OF POLYNOMIALS
       SUBROUTINE BOLLIN(A,AS,B,C,X,Y,Z1,Z2,Z3,N,UMAX)
DIMENSION A(MMAX,1),AS(NMAX,1),B(1),C(1),X(1),Y(1)
DIMENSION Z1(1),Z2(1),Z3(1)
   DOUBLE PRECISION AS, X, Y, Z1, Z2, Z3
TRANSFORM Z=TX TO MAKE OUTPUT A STATE
C
        CALL DAVISO(A,B,C,N,NMAX,MC)
    SAVE A USING AS
C
        DO 20 K=1,N
        DO 10 J=1,N
        AS(K,J)=A(K,J)
CONTINUE
10
20
    FIND DEN CHAR EQN COEF'S
C
    CALL DANSKY(AS,X,Y,Z1,N,NMAX)
SET AS=A AGAIN AND OVER WRITE A(K,MC) COLUMN WITH -B
Ċ
        DO 40 K=1,N
        DO 30 J=1,N
        AS(K,J)=A(K,J)
30
        AS(K,MC)=-B(K)
40
    FIND FIRST PART OF NUM CHAR EON
C
        CALL DANSKY (AS, X, Y, Z2, N, NMAX)
    SET AS=A AGAIN; COLLAPSE MC ROW AND COLUMN
C
        NM1=N-1
        DO 60 K=1,9M1
        K1=K
        HF(K.GE.MC) K1=K+1
        DO 50 J=1,NM1
        JI=J
        JF(J.GE.MC) J1=J+1
50
        AS(K,J)=A(K1,J1)
        CONTÍQUE
60
    FIND SECOND PART OF NUM CHAR EQN
    CALL DANSKY(AS,X,Y,Z3,NM1,NMAX)
SUBSTRACT FIRST PART FROM SECOND PART
DO 100 J=1,NM1
100
        Z2(J)=Z2(J)-Z3(J)
        RETURN
        END
```

### DAVISO

Davison

PURPOSE: Transform system to make output a state variable

USAGE: CALL DAVISO (A,B,C,N,NMAX,MC)

Where ' A - input system matrix which upon return is transformed system TAT 1

B - input system vector which upon return is transformed input vector TB

C - system output vector

N - order of A

NMAX - dimension of A in calling program > N

MC - position of maximum element in C vector

DOUBLE DIMENSION: A must be double dimensioned (NMAX, NMAX) in calling program

PROGRAM OUTPUT: If all N elements of C are zero the message "All elements of C are zero" is output and the pro-

gram is put in PAUSE

FIGURE 9.-DESCRIPTION OF SUBROUTINE DAVISO TRANSFER VARIABLES

```
TRANSFORM X(DOT)=AX+BU, Y=C(TRANSPOSE)X USING Z=TX SUCH
   THAT Y IS A STATE VARIABLE OF Z(DOT)=TAT(INVERSE)+TBU
       SUBROUTINE DAVISO(A, B, C, N, NHAX, MC)
       DIMENSION A(MMAX,1),B(1),C(1)
       DOUBLE PRECISION SUM
   FIND MAX ELEMENT IN C AS C(MC)
       CM=0.
       MC=0
      DO 5 J=1,N
IF(ABS(C(J)).LT.CM) GO TO 5
       CM=ABS(C(J))
       MC=J
       CONTINUE
٠5
       IF(MC.GT.0) GO TO 10
       WRITE(6,7)
       FORMAT(1x, 26HALL ELEMENTS OF C ARE ZERO)
7
       PAUSE
    PREMULT A BY T CHANGES MC ROW ONLY
C
10
       no .17 K=1,11
       SUM=0.
       DO 15 J=1,H
       SUM=SUM+DBLE(C(J)+A(J,K))
       A(MC,K)=SUM
17
    POST MULT A BY T INVERSE
C
               FOR J NOT = MC: \Lambda(K,J)=\Lambda(K,J)-\Lambda(K,MC)+C(J)/C(MC)
       PIVOT=1./C(MC)
       DO 30 J=1,N
       IF(J.EQ.MC) GO TO 30
       DO 25 K=1,N
       A(K,J)=A(K,J)-A(K,MC)*C(J)*P1VOT
25
       CONTINUE
30
                                 A(K,MC)=A(K,MC)/C(MC)
С
                FOR J=MC:
       DO 35 K=1,N
A(K,MC)=A(K,MC)*PIYOT
    PRE MULT B BY T CHANGES B(MC) ONLY
       SUM=0.
       DO 37 J=1,N
       SUM=SUM+DBLE(C(J)+B(J))
37
       B(MC)=SUM
       RETURN
       END
```

### FRPOLY

Frequency Response of Polynomials

PURPOSE: To evaluate system transfer function polynomials

to obtain system frequency response

USAGE: CALL FRPOLY (Z1,Z2,HZ,G,AMP,PHA,N)

Where Z1 - denominator polynomial, vector order N

Z2 - numerator polynomial, vector order N

HZ - frequency in hertz

G - system transfer function Z2(jHZ)/Z1(jHZ) evaluated at radian frequency HZ\*2π

AMP - transfer function amplitude, |G|

PHA - transfer function phase, ¿G degrees

N - order of Z1

COMPLEX: G must be declared complex in the calling program

DOUBLE PRECISION: Z1 and Z2 must be declared

double precision in the

calling program

NOTES: the Z1 and Z2 must be in the form:

$$z1 = \lambda^{n} + z1_{1}\lambda^{n-1} + \cdots + z1_{n}$$

$$z2 = z2_1\lambda^{n-1} + \cdots + z2_n$$

FIGURE 11.-DESCRIPTION OF SUBROUTINE FRPOLY TRANSFER VARIABLES

```
EVALUATE TRANSFER FUNCTION Z2(S)/Z1(S) FOR S=6.28+HZ+J
       SUBROUTINE FRPOLY(Z1, Z2, HZ, G, AMP, PHA, N)
      DIMENSION Z1(1), Z2(1)
DOUBLE PRECISION GT, WJ, SUM1R, SUM11, SUM2R, SUM21, ZZ1, ZZ2, ZI, ZZ
      COMPLEX G, SUM1, SUM2
      NM1=N-1
       SUM1R=Z1(N)
       SUM1 i=0.
       SUM2R=Z2(N)
       SUM2 != 0.
      GT=1.
      NJ=HZ*6.2831853
1
       KK=2
       IF(NM1.EQ.0) GO TO 40
       DO 35 K=1,NM1
      NWK=N-K
       GT=GT+WJ
       ZZ1=Z1(NMK)+GT
      ZZ2=Z2(NMK)*GT
       GO TO (5,10,3,8),KK
       ZZ1=-ZZ1
3
       ZZ2=-ZZ2
5
       SUM1R=SUM1R+ZZ1
       SUM2R=SUM2R+ZZ2
      GO TO 30
       ZZ1=-ZZ1
8
       ZZ2=-ZZ2
       SUM11=SUM11+ZZ1
10
       SUM2 = SUH12 1+ZZ2
30
       KK=KK+1
       1F(KK.GT.4) KK=1
35
       CONTINUE
   ADD ON S**N TO DEN SUM1
C
       SUM1=CMPLX(SNGL(SUM1R), SNGL(SUM11))+GT+WJ+(CMPLX(0.,1.))+*(KK-1)
SUM2=CMPLX(SNGL(SUM2R), SNGL(SUM2I))
40
       G=SUM2/SUM1
       AMP=CABS(G)
       PHA=ATAN2(AIMAG(G), REAL(G)) *57.29578
       RETURN
       END
```

# SYSTEM STATE VARIABLE EQUATIONS

$$\dot{x} = Ax + Bu, y = C^{t}x$$

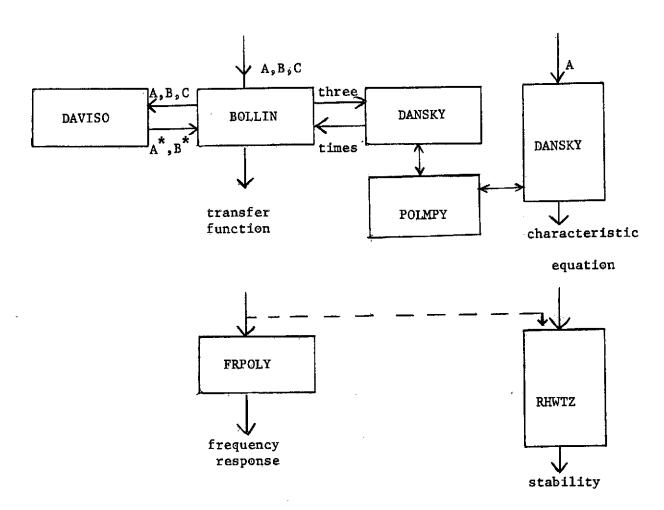


FIGURE 13.-FLOW CHART FOR FORTRAN SUBROUTINES

```
SAMPLE PROBLEM MAIN PROGRAM
             DIMENSION A(3,3), AS(3,3), B(3), C(3), Z1(3), Z2(3), Z3(3), X(3), Y(3)
             DOUBLE PRECISION AS, Z1, Z2, Z3, X, Y
             COMPLEX G
             DATA A/0.,0.,-36.,1.,0.,-21.,0.,1.,-7./
             DATA B/0.,0.,1./,C/6.,1.,O./,HZ,N,NMAX/1.,3,3/
            WRITE(6,1) ((A(1,J),J=1,N),I=1,N)
FORMAT('A=',/,1P3E12.3,/,1P3E12.3)
WRITE(6,2) (B(J),J=1,N)
FORMAT('B VECTOR=',1P3E12.3)
   2
             WRITE(6,3) (C(J),J=1,N)
FORMAT(' C VECTOR=',1P3E12.3)
CALL BOLLIN(A,AS,B,C,X,Y,Z1,Z2,Z3,N,NMAX)
   3
             WRITE(6,10) (Z1(J), J=1,N)
FORMAT(' DENOMINATOR=',1P3E12.3)
   10
             WRITE(6,20) (Z2(J),J=1,N)
FORMAT(' NUMERATOR=',1P3E12.3)
CALL FRPOLY(Z1,Z2,HZ,G,AMP,PHA,N)
   20
           WRITE(6,30) HZ,G,AMP,PHA
FORMAT('AT',F4.1,' HERTZ THE TRANSFER FUNCTION =',-
1 1P2E12.3,/,' AMPLITUDE=',1PE12.3,' PHASE=',1PE12.3)
CALL RHWTZ(Z1,N,M)
   30
             WRITE(6,40) M
FORMAT(' NUMBER OF UNSTABLE ROOTS=',15)
40
             STOP
             END
```

FIGURE 14, - FORTRAN listing for sample problem main program

```
0.000
               1.000E 00
                             0.000
                            1.000E 00
  0.000
               0.000
 -3.600E 01
             -2.100E 01
                           -7.000E 00
B VECTOR=
             0.000
                          0.000
                                        1.000E 00
                          1.000E 00
             6.000E 00
C VECTOR≈
                                        0.000
DENOMINATOR=
               7.000E 00 2.100E 01
                                          3.600E 01
NUMERATOR≈ -2.220E-16
NUMERATOR = -2.220E-16 1.000E 00 6.000E 00
AT 1.0 HERTZ THE TRANSFER FUNCTION = -3.048E-02 -1.142E-02
AMPLITUDE=
              3.255E-02 PHASE= -1.595E 02
NUMBER OF UNSTABLE ROOTS=
```